

Fundamental Study of a 7-element Fuel Injector Configuration for Gas Turbine Combustors - A Look at Cold Flow and Burning Measurements

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Minneapolis, MN, 20-22 May 2018

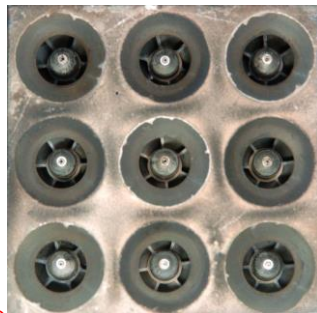
Objectives



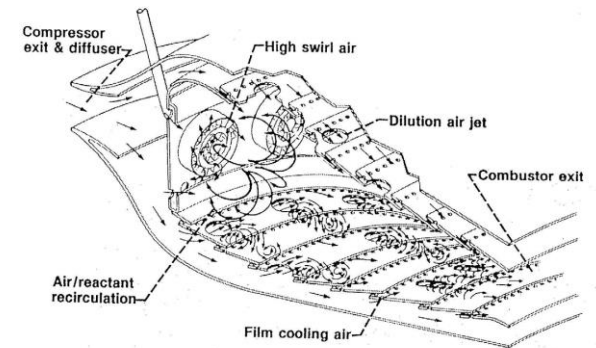
- Parametric study to help guide injector design for Low-NO_x emissions for aircraft gas turbine engines
- Study fuel-air mixing and combustion using Lean Direct Injection (LDI) as platform. LDI strategy is to inject and mix quickly the fuel and air for uniform distribution to avoid near-stoichiometric burning that would lead to high NO_x concentrations
- One goal for the 7-point LDI experiments is to quantify the effect of air swirl angle on recirculation, fuel-air mixing, combustion emissions and flame tube combustor operability



7-pt



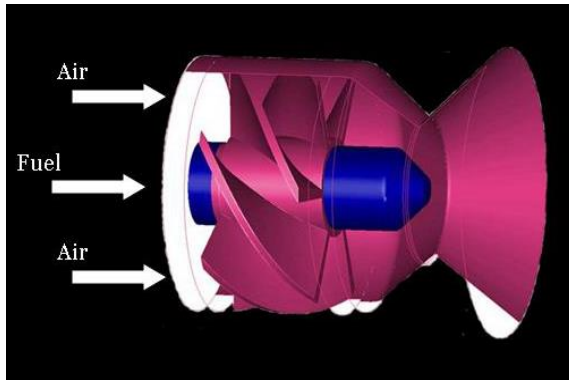
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- FULLY 3-DIMENSIONAL FLOW
- HIGH TURBULENCE LEVELS
- CHEMICAL REACTION/HEAT RELEASE
- 2 PHASE WITH VAPORIZATION

LDI Hardware Details

Baseline LDI element



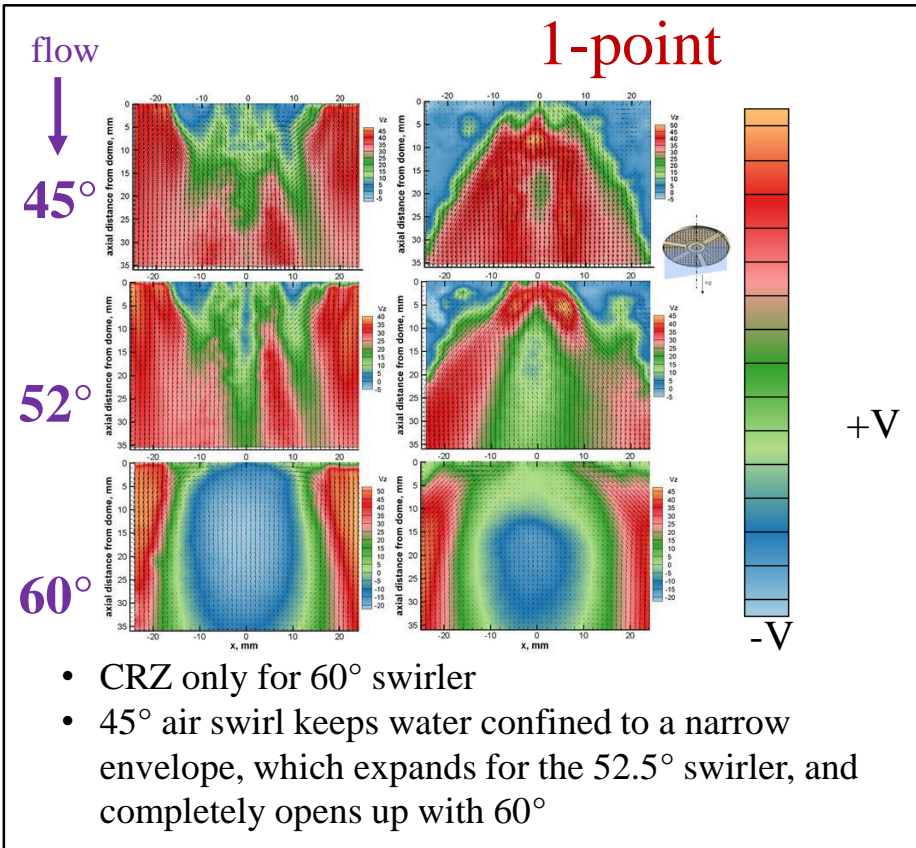
- Six helical angled vanes
- Simplex atomizing nozzle
- Converging-Diverging Venturi

Swirlers: 45°, 52°, 60°
Swirl #s: 0.59, 0.77, 1.02



- 76.2 mm overall diameter
- 23.8 mm between adjacent elements
- Center can be offset upstream to act as a “pilot”

Brief overview of previous LDI tests



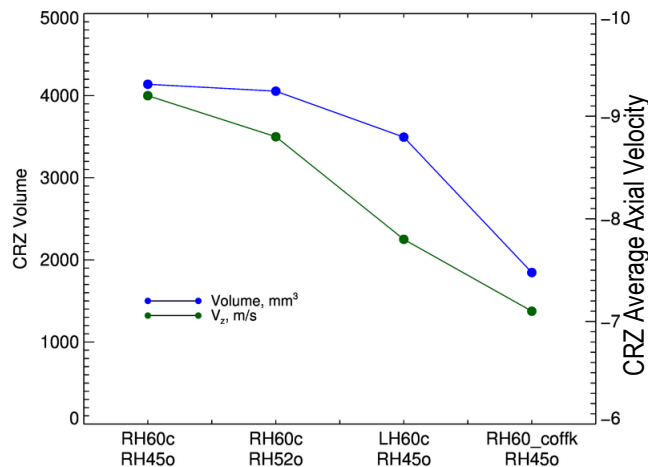
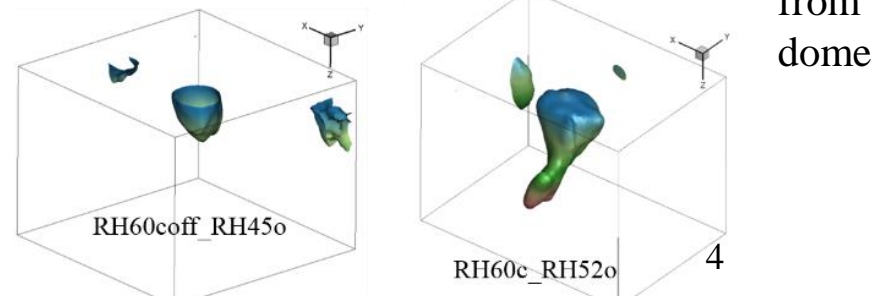
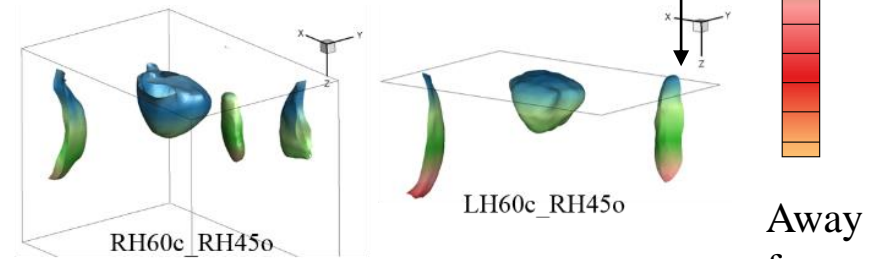
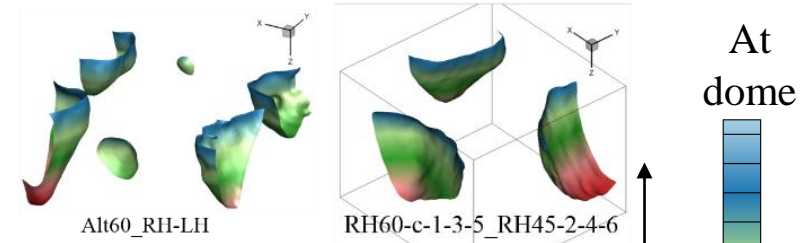
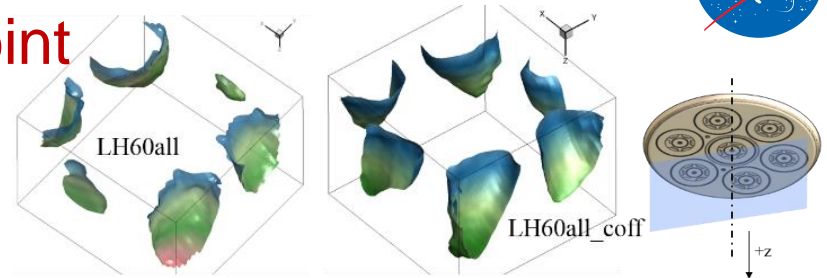
7-point

flow ↓

Re: Center swirler CRZ

Without CRZ

With CRZ

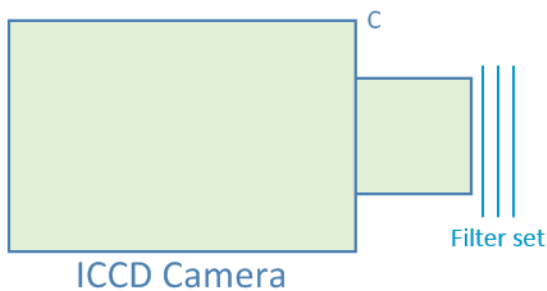


Current Study, counter-swirling configuration

- Center swirler: counterclockwise 60°
- Outer swirlers: clockwise 52°
- Non-reacting 2D velocity – determine extent of central recirculation zone
- Chemiluminescence imaging of intermediate combustion species, C_2^* , CH^* , OH^*
- Flame spectra



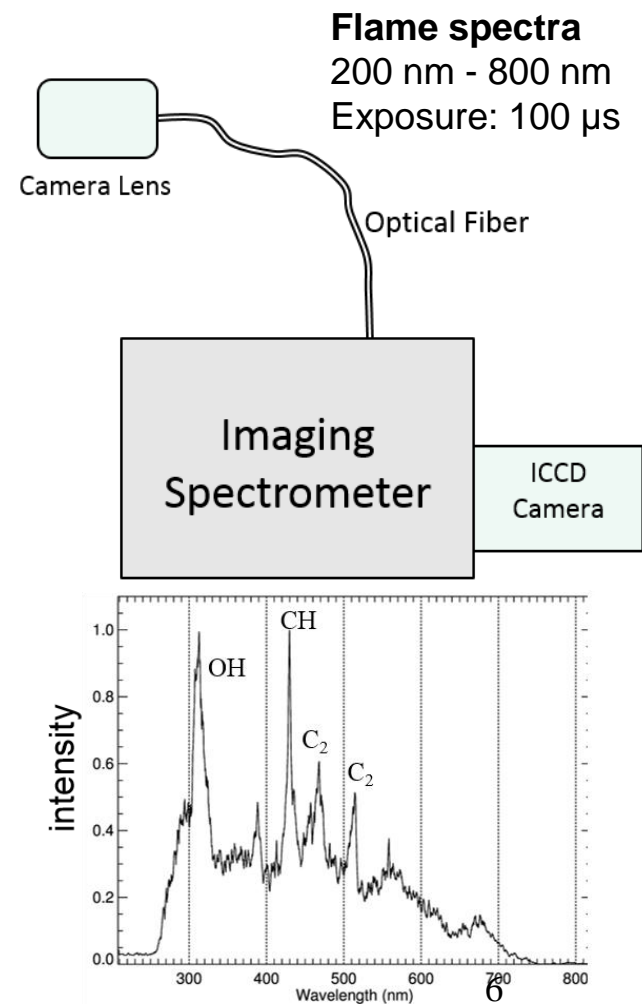
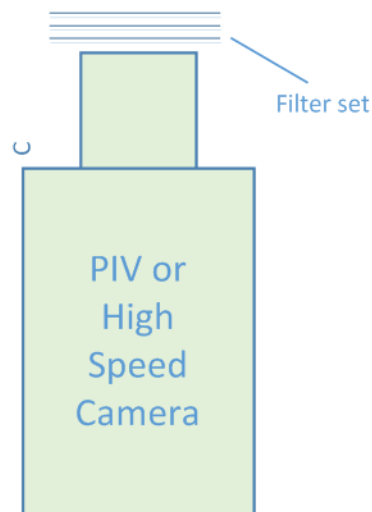
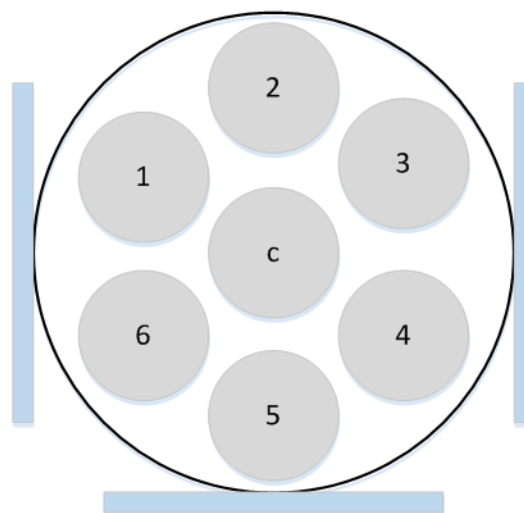
Setup used for 7-LDI testing



ICCD camera: 1k x 1k pixels
 UV intensifier, Super Blue Slow Gate
 C_2^* chemiluminescence~514-nm
 gate: 500-ns

High speed camera: 1k x 1k pixels
 40-kHz, 320px x 368 px, exposure: 25- μ s
 C_2^* chemiluminescence~514-nm

PIV camera:
 15 image pairs/s



Test Matrix, Data Collection and Processing

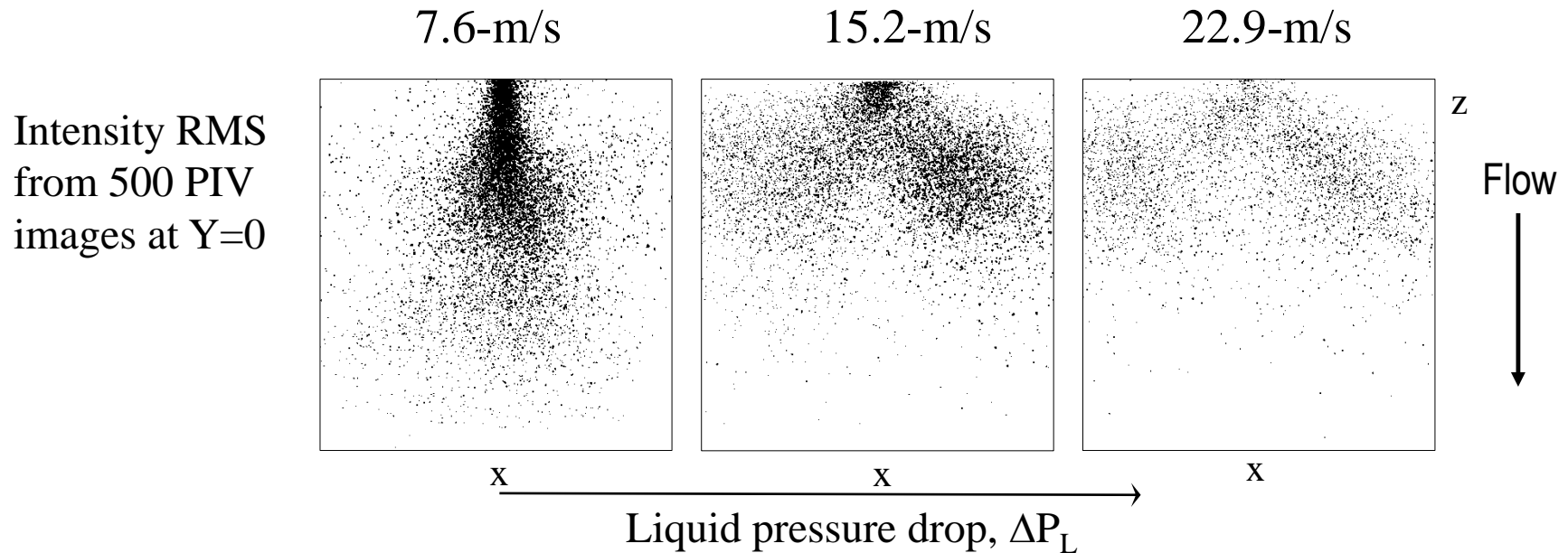
$$T_{\text{inlet}} = 800\text{K}, P_{\text{inlet}} = 5\text{-kPa}$$

| | | | | | | |
|------------------|-------------------------------|------|------|------|------|---|
| <i>Cold flow</i> | $u_{\text{ref}}, \text{ m/s}$ | 7.6 | | 15.2 | 22.9 | Constant: $\phi \cong 0.35$ |
| <i>Burning</i> | $u_{\text{ref}}, \text{ m/s}$ | 9.1 | 10.7 | 12.2 | 13.7 | Constant: $\phi = 0.45$ |
| | ϕ | 0.43 | 0.45 | 0.48 | 0.50 | Constant: $u_{\text{ref}} = 10.7 \text{ m/s}$ |

- PIV: 500 image pairs, $\sim 15\text{-Hz}$, 6-ns/laser pulse, traverse y- in 1-mm increments
 - Water seeding through center nozzle
 - Cross-correlation processing for instantaneous, average, and RMS 2D vector fields
- High speed camera: ~ 48000 frames @ 40-kHz frame rate, 25- μs exposures
 - Chemiluminescence imaging—line of sight
 - C2 filter: centered at 510-nm, 8-nm FWHM, 50% transmission
 - Processing: average intensity, RMS intensity
- ICCD camera: 500 frames @ 25-Hz frame rate, 500-ns gate
 - Chemiluminescence imaging—line of sight
 - C2 filter: centered at 511-nm, 11.5-nm FWHM, 50% transmission
 - Processing: average intensity, RMS intensity

On seeding water through nozzle

- Keeps windows clean—air seeding typically does not
- Whether tracks air or water (or both) depends on atomization
- Fuel distribution similar during non-combusting flow

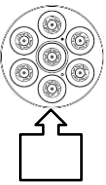


Flow number, $FN_{US} = \text{flow rate, pph} \times (\Delta P_L)^{-0.5}$

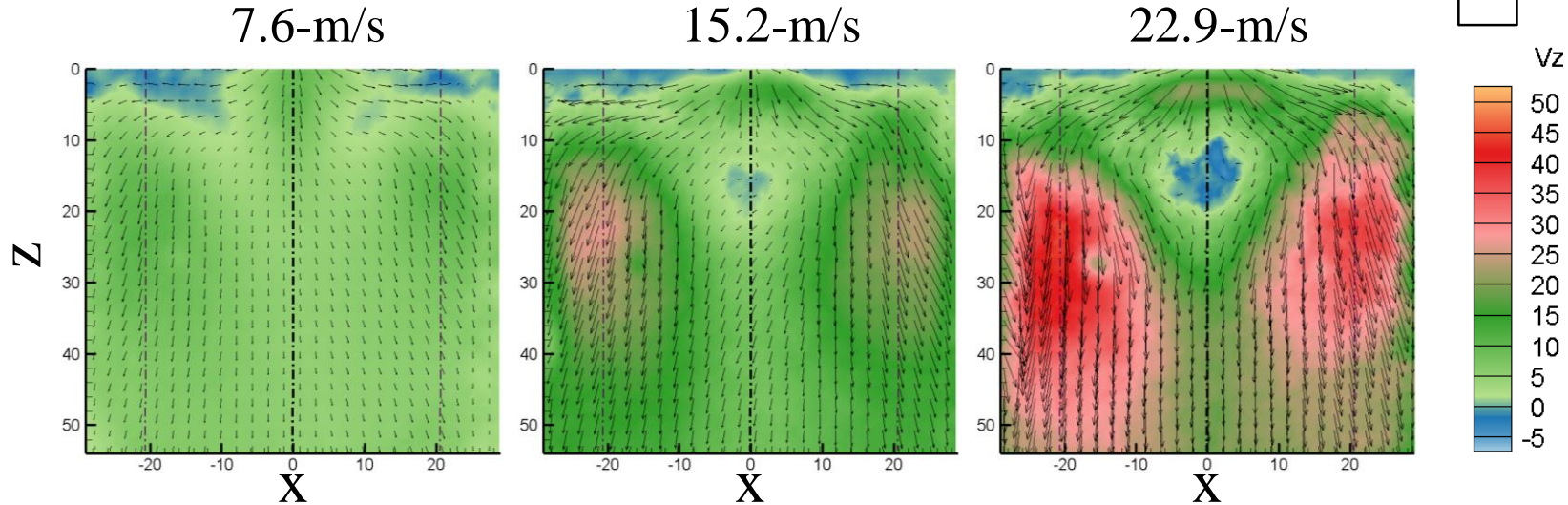
Atomization improves as ΔP_L increases: $SMD \propto (\Delta P_L)^{-0.375}$

Spray penetration $S \propto (\Delta P_L)^{-0.27}$

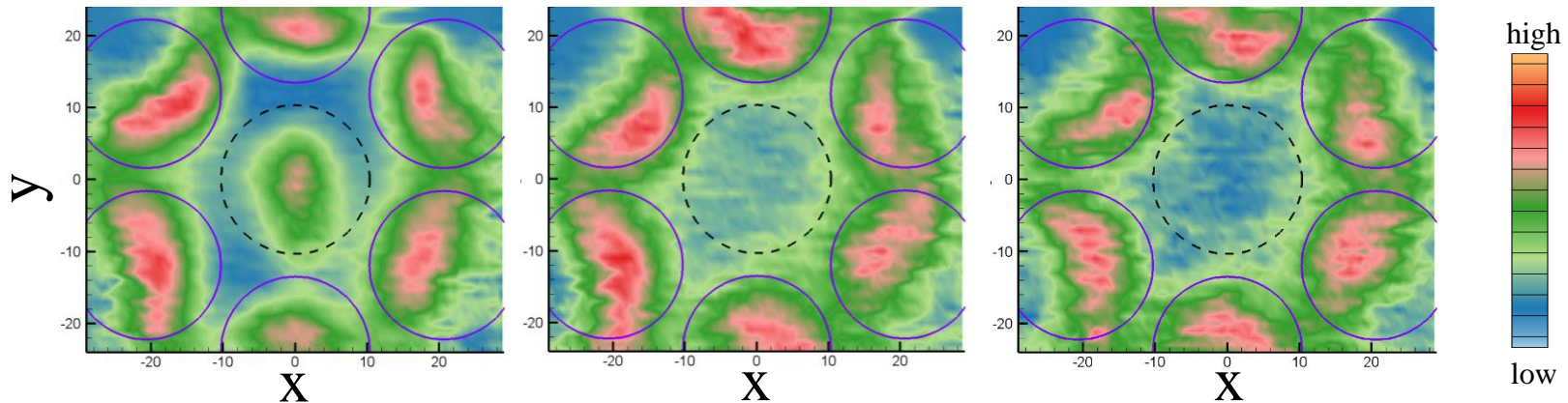
Cold flow PIV results: mean axial velocity fields



$Y = 0$
Flow:
Top \rightarrow bottom



$Z = 10$
Flow:
Normal to page

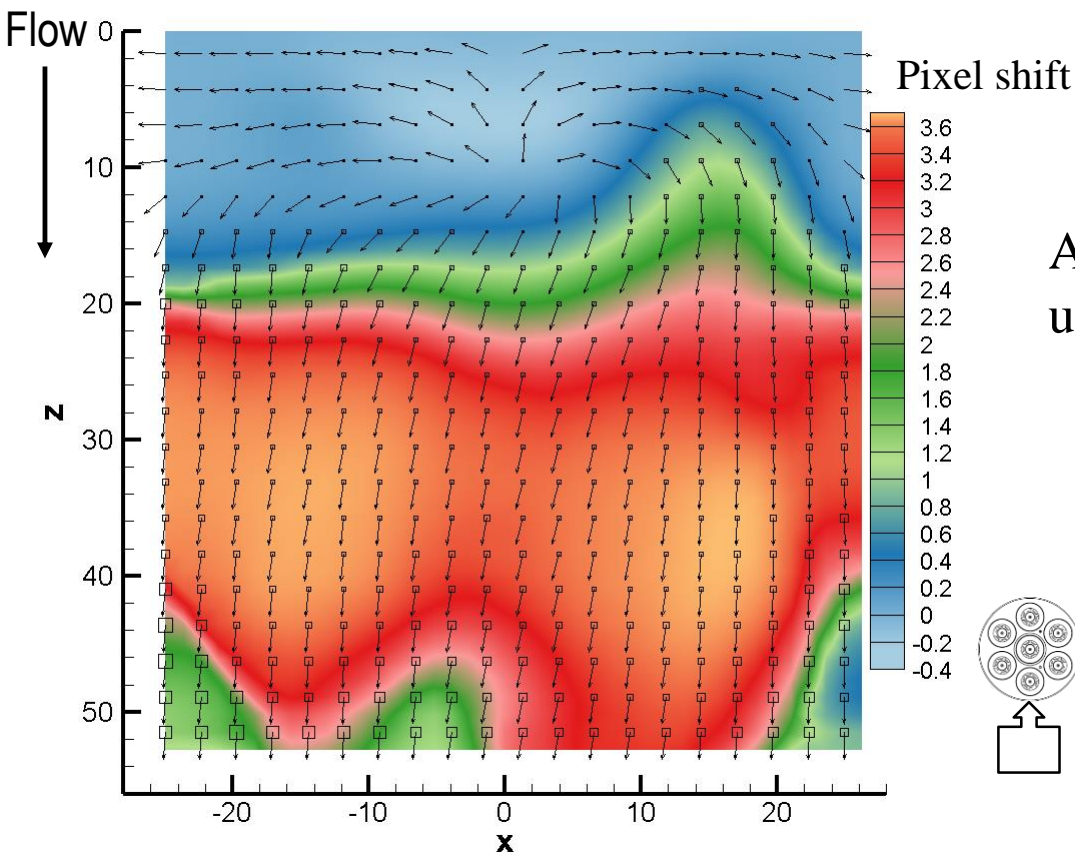


- Increased reference velocity—better tracks air near injector dump plane
- Lowest reference velocity does not indicate recirculation zone in cold flow
- Only highest reference velocity shows distinct CRZ

Combusting results: Tracking C_2^* chemiluminescence using high speed camera

Recirculation zone observed, relatively weak ($1/9^{\text{th}}$ of max downstream rate).
Only in center of field—likely due to 60° air swirler

Relative magnitude of recirculation on order of cold flow maximum reference velocity



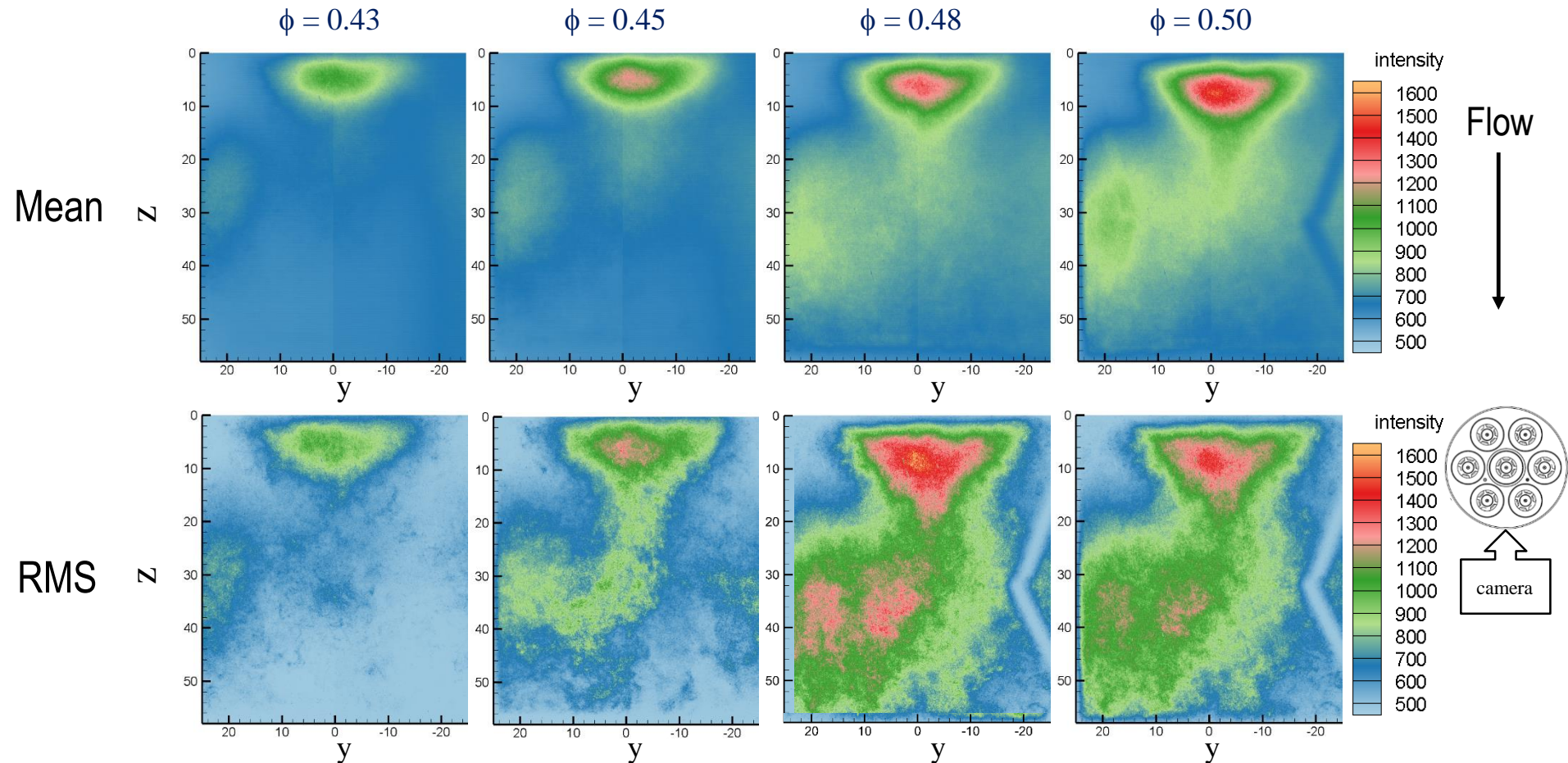
$$U_{\text{ref}} = 13.7\text{-m/s}, \phi = 0.5$$

Average of 48,000 frames, processed
using time-series PIV



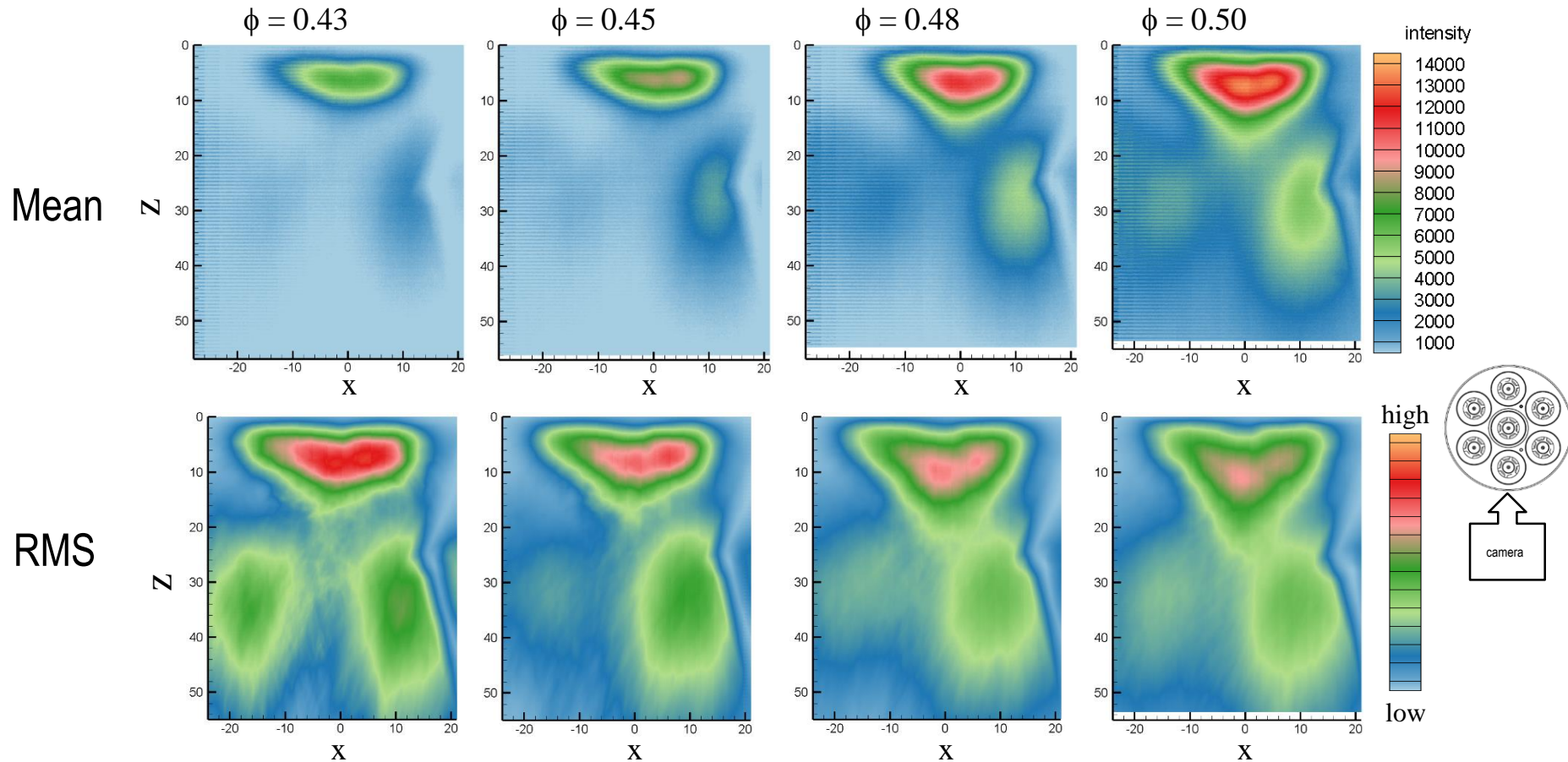
Combusting results: Equivalence Ratio Effect, $U_{\text{ref}} = 10.7\text{-m/s}$

C_2^* chemiluminescence image statistics—ICCD camera



- C_2^* intensity increases with equivalence ratio
- highest signal occurs immediately downstream of the dump plane and near center
- Somewhat asymmetric downstream

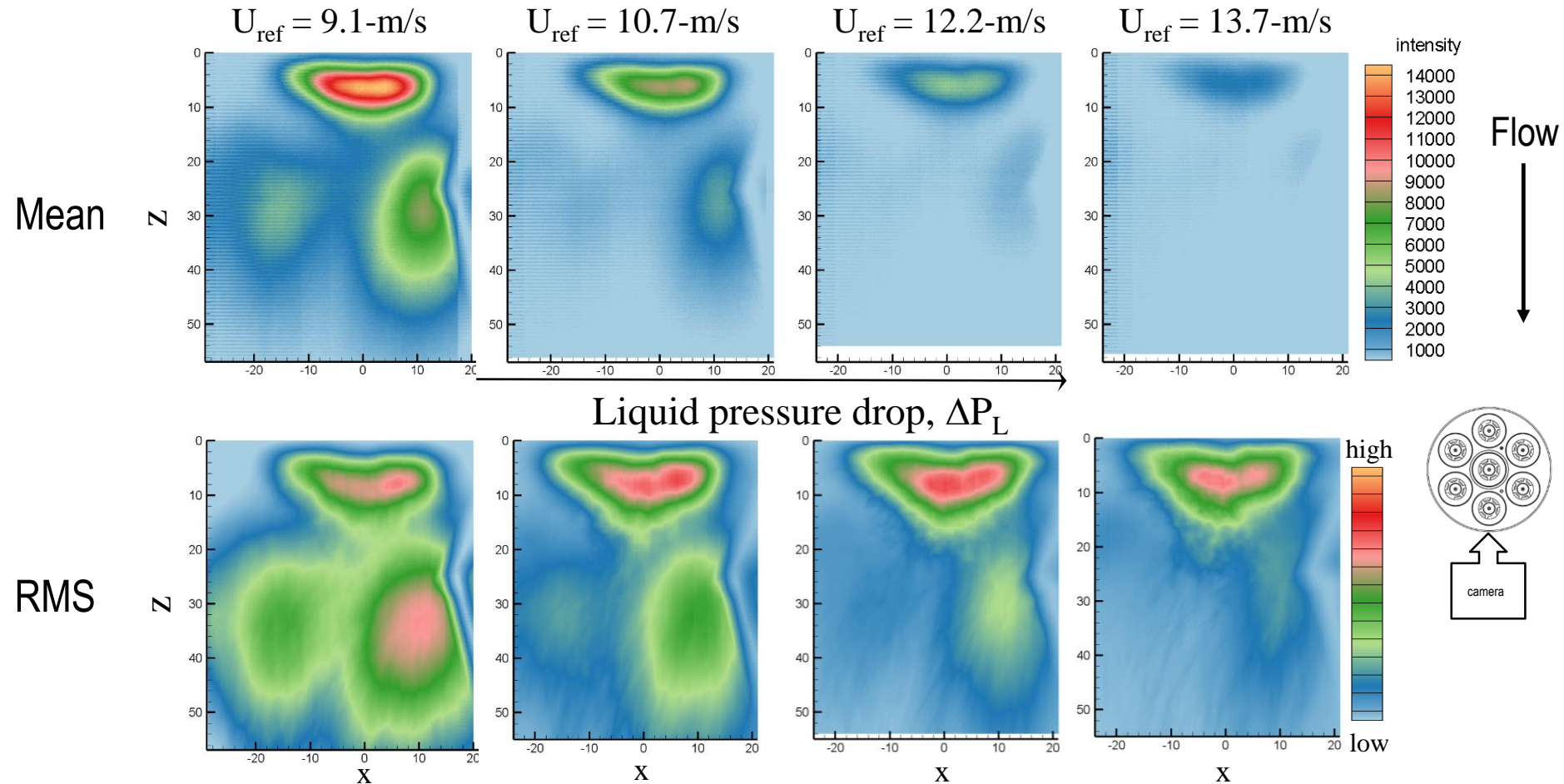
C_2^* chemiluminescence image statistics—High Speed camera



- C_2^* intensity increases with equivalence ratio
- highest signal occurs immediately downstream of the dump plane and near center
- Somewhat asymmetric downstream

Combusting results: Reference Velocity Effect, $\phi = 0.45$

C_2^* chemiluminescence image statistics—High Speed camera



- overall signal decreases with increasing reference velocity
- better fuel atomization and fuel vaporization
- Increase in air flow \rightarrow higher turbulence intensity, increased fuel-air mixing

Summary



We presented data from our most recent parametric tests to characterize the flow field of a NASA 7-point LDI injector

- counterclockwise 60° center swirler surrounded by six clockwise 52° swirlers.
- 2D non-combusting velocity fields
 - Highest reference velocity conditions are best indicator of whether a CRZ will develop during combustion.
 - This configuration CRZ amongst smallest compared to previous configurations
- chemiluminescence data in the form of C_2^* imaging and flame spectra.
 - for a given air flow rate, the chemiluminescence signal increases with increasing fuel flow rate under fuel-lean conditions.
 - at fixed equivalence ratio, the chemiluminescence signal decreases with increasing air flow rate (reference velocity).
 - This counterswirl configuration generates an asymmetric distribution of C_2^* in the downstream region of the outer injectors. The co-swirl configuration did not.



Acknowledgment

The NASA Transformational Tools and Technologies
Project of the Aeronautics Research Mission
Directorate supported this work.